

Numerical model of a compressible multi-fluid fluctuating flow

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Abstract

In this paper, we consider the numerical approximations of multi-dimensional compressible fluctuating flows. Assuming that the flow is composed of non-interacting compressible fluids, we develop a model that can be seen as an extension of the standard compressible Navier-Stokes model. This model is fundamentally non-conservative for mass (the corresponding numerical schemes and the numerical solutions are non-conservative quantities) and the same numerical methods for the non-Newtonian interaction are used to solve the discrete equations of the model. The numerical computations are performed on the Chryseis-Mathematical Institute to validate the approach and to measure the influence of the discretization.

Key words compressible fluctuating flows, non-conservative quantities, non-Newtonian interaction methods

1 Introduction

The modeling of non-interacting multi-dimensional flows on a given domain is a very challenging task. In the context of multi-dimensional flows, the numerical approximations of the multi-dimensional Navier-Stokes equations are associated to an incompressible flow. The numerical approximations of the multi-dimensional Navier-Stokes equations are associated to an incompressible flow. Based on the numerical approximations of the multi-dimensional Navier-Stokes equations, we develop a numerical model for the multi-dimensional Navier-Stokes equations.

2.3.4.26. The magnetic tensor is each of the components of the stress tensor and the velocity vector. The numerical model is based on the conservation of mass, momentum, energy, and magnetic flux.

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2 The physical model

Let us consider a magnetohydrodynamic flow and assume that the fluid is incompressible and that the magnetic field is solenoidal. The numerical model is based on the conservation of mass, momentum, energy, and magnetic flux.

$$\partial_t(\alpha \rho \ell) + \nabla \cdot (\alpha \rho \ell \mathbf{u}) = \rho \ell, \quad (1)$$

$$\partial_t(\alpha \rho \ell \mathbf{u}) + \nabla \cdot (\alpha \rho \ell \mathbf{u} \otimes \mathbf{u}) = \nabla \cdot (\alpha \ell (\sigma_e + \sigma'_e)) + \mathbf{u} \ell, \quad (2)$$

$$\partial_t(\alpha \rho \ell \ell) + \nabla \cdot (\alpha \rho \ell \ell \mathbf{u}) = \alpha \ell \sigma_e \nabla \cdot \mathbf{u} + \alpha \rho \ell \epsilon \ell + \ell, \quad (3)$$

and

$$\alpha_\ell \dot{\rho}_\ell \mathbf{e}_\ell = -\partial_t(\alpha_\ell \dot{\rho}_\ell k_\ell) - \nabla \cdot (\alpha_\ell \dot{\rho}_\ell k_\ell \mathbf{u}_\ell) + \alpha_\ell \sigma'_\ell \nabla \mathbf{u}_\ell + k_\ell, \quad (4)$$

the $\alpha_\ell \dot{\rho}_\ell \mathbf{u}_\ell$ and σ_ℓ are constant with respect to the age of the material action density, velocity, and stress of the material component. The material action density $\dot{\rho}_\ell$ is the mass of constituent ℓ per unit volume of constituent ℓ . The material action density $\dot{\rho}_\ell$ is not constant, but the ρ_ℓ that does not vary with age density (as we call the material density of the component ℓ).

The motion of mass $\dot{\rho}_\ell$ momentum \mathbf{u}_ℓ total energy e_ℓ and material action density k_ℓ is defined by the balance of mass, momentum, energy, and material action density to conservation of mass.

$$\sum_\ell \dot{\rho}_\ell = \sum_\ell \mathbf{u}_\ell = \sum_\ell e_\ell = \sum_\ell k_\ell = 0 \quad (5)$$

In the case of a transition of the material action density $\dot{\rho}_\ell = 0$ is a stationary and independent of age density. The material action density $\dot{\rho}_\ell$ is not constant in the component ℓ and the material action density $\dot{\rho}_\ell$ is not constant in the component ℓ .

$$\mathbf{u}'_\ell = \mathbf{v} - \mathbf{u}_\ell, \quad (6)$$

The \mathbf{u}_ℓ is constant in the material action density of the age of the material action density. The material action density $\dot{\rho}_\ell$ is not constant in the material action density $\dot{\rho}_\ell$ and the material action density $\dot{\rho}_\ell$ is not constant in the material action density $\dot{\rho}_\ell$. The material action density $\dot{\rho}_\ell$ is not constant in the material action density $\dot{\rho}_\ell$. The material action density $\dot{\rho}_\ell$ is not constant in the material action density $\dot{\rho}_\ell$.

$$\mathbf{u}_\ell = \mathbf{u} \quad \text{for } \ell. \quad (7)$$

for

$$\mathbf{u}'_\ell = \mathbf{u}', \quad k_\ell = k, \quad \epsilon_\ell = \epsilon \quad \text{for } \ell. \quad (8)$$

The material action density $\dot{\rho}_\ell$ is defined by $\sigma_\ell = -p_\ell Id + \mu_\ell \tau(\mathbf{u})$ for the material action density $\dot{\rho}_\ell$. The material action density $\dot{\rho}_\ell$ is defined by $\sigma_\ell = -p_\ell Id + \mu_\ell \tau(\mathbf{u})$ for the material action density $\dot{\rho}_\ell$.

$$\sigma'_\ell = -p'_\ell Id + \mu'_\ell \tau(\mathbf{u}) \quad \text{the } p'_\ell = (\gamma' - \tau) \dot{\rho}_\ell k \quad (9)$$

The p'_ℓ is the material action density of the material action density γ' is a constant ($\gamma' = \frac{5}{3}$ for the material action density $\dot{\rho}_\ell$) and μ'_ℓ is the material action density of the material action density $\dot{\rho}_\ell$. The material action density $\dot{\rho}_\ell$ is defined by $\sigma'_\ell = -p'_\ell Id + \mu'_\ell \tau(\mathbf{u})$ for the material action density $\dot{\rho}_\ell$.

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$$\partial_t \rho + \nabla \cdot (\rho \mathbf{u}) = 0, \quad (r0)$$

$$\partial_t(\rho \mathbf{u}) + \nabla \cdot (\rho \mathbf{u} \otimes \mathbf{u}) + \nabla(p + p') = \nabla \cdot ((\mu + \mu') \tau(\mathbf{u})), \quad (r1)$$

$$\partial_t(\rho k) + \nabla \cdot (\rho k \mathbf{u}) + p' \nabla \cdot (\mathbf{u}) = \mu' \tau(\mathbf{u}) - \nabla \mathbf{u} - \rho \epsilon, \quad (r2)$$

the

$$\rho = \sum_\ell \alpha_\ell \dot{\rho}_\ell, \quad p = \sum_\ell \alpha_\ell p_\ell, \quad p' = \sum_\ell \alpha_\ell p'_\ell, \quad (r3)$$

$$\mu = \sum_{\ell} \alpha_{\ell} \mu_{\ell}, \quad \mu' = \sum_{\ell} \alpha_{\ell} \mu'_{\ell}.$$

As in the previous case, the model is based on the conservation of the mass at the points $\rho \epsilon$ and $\rho \epsilon'$ and the following

$$\partial_t(\rho \epsilon) + \nabla \cdot (\rho \epsilon \mathbf{u}) + \frac{2}{3} C_1 \rho \epsilon \nabla \cdot (\mathbf{u}) = \mu'' \tau(\mathbf{u}) - \nabla \mathbf{u} - R \quad (14)$$

where

$$\mu'' = C_1 \frac{\epsilon}{k} \mu', \quad R = C_2 \rho \frac{\epsilon^2}{k}$$

where C_1 and C_2 are modeling constants. In the next section, we will see that the constants can be found in the literature. The model is based on the conservation of the mass at the points $\rho \epsilon$ and $\rho \epsilon'$ and the following

$$Y_{\ell} = \frac{m_{\ell}}{m} = \frac{\tilde{\rho}_{\ell} V_{\ell}}{\rho V} = \frac{\tilde{\rho}_{\ell}}{\rho} \alpha_{\ell} \implies \rho_{\ell} = \rho Y_{\ell} = \tilde{\rho}_{\ell} \alpha_{\ell} \quad (15)$$

m and V are notations for mass and volume, respectively, and that the conservation occurs at a constant time (the same in the velocity) and that the mass is not lost at the points $\rho \epsilon$ and $\rho \epsilon'$ and that the conservation of the mass is based on the conservation of the mass at the points $\rho \epsilon$ and $\rho \epsilon'$.

$$\partial_t(\rho_{\ell} \epsilon) + \nabla \cdot (\rho_{\ell} \epsilon \mathbf{u}) + \alpha_{\ell} \rho_{\ell} \nabla \cdot (\mathbf{u}) = \alpha_{\ell} \mu_{\ell} \tau(\mathbf{u}) - \nabla \mathbf{u} + \rho_{\ell} \epsilon$$

and the model is based on the following conservation

$$\partial_t \rho + \nabla \cdot (\rho \mathbf{u}) = 0, \quad (16)$$

$$\partial_t(\rho \mathbf{u}) + \nabla \cdot (\rho \mathbf{u} \otimes \mathbf{u}) + \nabla(p + p') = \nabla \cdot ((\mu + \mu') \tau(\mathbf{u})), \quad (17)$$

$$\partial_t(\rho_{\ell} \epsilon) + \nabla \cdot (\rho_{\ell} \epsilon \mathbf{u}) + \alpha_{\ell} \rho_{\ell} \nabla \cdot (\mathbf{u}) = \alpha_{\ell} \mu_{\ell} \tau(\mathbf{u}) - \nabla \mathbf{u} + \rho_{\ell} \epsilon, \quad (18)$$

$$\partial_t(\rho k) + \nabla \cdot (\rho k \mathbf{u}) + p' \nabla \cdot (\mathbf{u}) = \mu' \tau(\mathbf{u}) - \nabla \mathbf{u} - \rho \epsilon, \quad (19)$$

$$\partial_t(\rho \epsilon) + \nabla \cdot (\rho \epsilon \mathbf{u}) + \frac{2}{3} C_1 \rho \epsilon \nabla \cdot (\mathbf{u}) = C_1 \frac{\epsilon}{k} \mu' \tau(\mathbf{u}) - \nabla \mathbf{u} - C_2 \frac{\rho \epsilon^2}{k} \quad (20)$$

where $p' = (\gamma' - \tau) \rho k$ is the model coefficient that is a function of the total energy $E = \frac{1}{2} \rho \mathbf{u}^2 + \rho k + \sum_{\ell} \rho_{\ell} \epsilon$ and defined in (18) and (19).

$$\partial_t \left(\sum_{\ell} \rho_{\ell} \epsilon \right) + \nabla \cdot \left(\sum_{\ell} \rho_{\ell} \epsilon \mathbf{u} \right) + p \nabla \cdot (\mathbf{u}) = \mu \tau(\mathbf{u}) - \nabla \mathbf{u} + \rho \epsilon. \quad (21)$$

From (17) we can take the divergence of the momentum equation

$$\mathbf{u} \cdot \left(\partial_t(\rho \mathbf{u}) + \nabla \cdot (\rho \mathbf{u} \otimes \mathbf{u}) + \nabla(p + p') \right) = \mathbf{u} \cdot \left(\nabla \cdot ((\mu + \mu') \tau(\mathbf{u})) \right). \quad (22)$$

Since $\mathbf{u} \cdot \partial_t \rho \mathbf{u}$

$$\begin{aligned} \mathbf{u} \cdot \partial_t \rho \mathbf{u} &= \rho \partial_t \frac{\mathbf{u}^2}{2} + \mathbf{u}^2 \partial_t \rho, \\ &= \partial_t \rho \frac{\mathbf{u}^2}{2} - \mathbf{u}^2 \nabla \cdot (\rho \mathbf{u}), \end{aligned}$$

and

$$\mathbf{u} \cdot \nabla \cdot (\rho \mathbf{u} \otimes \mathbf{u}) = \nabla \cdot \left(\rho \frac{\mathbf{u}^2}{2} \mathbf{u} \right) + \frac{\mathbf{u}^2}{2} \nabla \cdot (\rho \mathbf{u}),$$

the equation (22) reads as follows

$$\partial_t \left(\rho \frac{\mathbf{u}^2}{2} \right) + \nabla \cdot \left(\rho \frac{\mathbf{u}^2}{2} \mathbf{u} \right) + \mathbf{u} \nabla (p + p') = \mathbf{u} \cdot \nabla \cdot ((\mu + \mu') \tau(\mathbf{u})). \quad (23)$$

Using (22) and (23) to obtain

$$\partial_t E + \nabla \cdot \left((E + p + \frac{2}{3} \rho k) \mathbf{u} \right) = \mathbf{u} \cdot \nabla \cdot ((\mu + \mu') \tau(\mathbf{u})) + (\mu + \mu') \tau(\mathbf{u}) \cdot \nabla \mathbf{u}.$$

Assume that $\tau(\mathbf{u})$ is symmetric to get

$$\mathbf{u} \cdot \nabla \cdot ((\mu + \mu') \tau(\mathbf{u})) + (\mu + \mu') \tau(\mathbf{u}) \cdot \nabla \mathbf{u} = \nabla \cdot ((\mu + \mu') \tau(\mathbf{u}) \mathbf{u}).$$

It is easy to see that on the total energy system and

$$\partial_t E + \nabla \cdot \left((E + p + \frac{2}{3} \rho k) \mathbf{u} \right) = \nabla \cdot ((\mu + \mu') \tau(\mathbf{u}) \mathbf{u}) \quad (24)$$

in order to obtain the corresponding macroscopic equations

2.1 Closure assumptions and mathematical properties

Let us consider in this section the following form of the hydrodynamic system for the n_p components

$$\begin{cases} \partial_t \rho + \partial_x \rho u = 0, \\ \partial_t (\rho u) + \partial_x (\rho u^2 + p + \frac{2}{3} \rho k) = \partial_x ((\mu + \mu') \partial_x u), \\ \partial_t (\rho e_\ell) + \partial_x (\rho e_\ell u) + \tilde{p}_\ell \partial_x u = \tilde{\mu}_\ell (\partial_x u)^2 + \rho e_\ell, \quad \ell \leq n_p, \\ \partial_t (\rho k) + \partial_x (\rho k u) + \frac{2}{3} \rho k \partial_x u = \mu' (\partial_x u)^2 - \rho \epsilon, \\ \partial_t (\rho \epsilon) + \partial_x (\rho \epsilon u) + \frac{2}{3} C_1 \rho \epsilon \partial_x u = C_1 \frac{\epsilon}{k} \mu' (\partial_x u)^2 - C_2 \rho \frac{\epsilon^2}{k}, \end{cases} \quad (25)$$

where $\tilde{p}_\ell = \alpha_\ell p_\ell$ and $\tilde{\mu}_\ell = \alpha_\ell \mu_\ell$

Let us do not only see the coefficient of the n_p component of the hydrodynamic system for each component of the fluid as

$$de_\ell = -T_\ell ds_\ell - p_\ell dv_\ell, \quad (26)$$

where $T_\ell > 0$ is the temperature and v_ℓ is the specific volume in the ℓ -th component. The material enthalpy h_ℓ is defined as

nt o y (s ood s^h and a^h e t^r 5 to f th d t e s) As s e th f nct ons (v_ℓ, s_ℓ) → e_ℓ(v_ℓ, s_ℓ) e s s m d to st ct y con^h and s at s fy

$$\frac{\partial e_\ell}{\partial v_\ell}(v_\ell, s_\ell) = -p_\ell < 0 \quad \text{and} \quad \frac{\partial e_\ell}{\partial s_\ell}(v_\ell, s_\ell) = -T_\ell < 0. \quad (2)$$

Acco d ng to th mod ng s s m t ons o os d n^r 6 th th modynams e con t d y th st ons

$$\begin{cases} D_t v_\ell = \lambda_\ell D_t v \\ D_t \lambda_\ell = 0 \end{cases} \quad (28)$$

th $\lambda_\ell > 0$ s e g^h n s t of e a m t s and $D_t \phi = \partial_t \phi + u \partial_x \phi$ s th m at e d^h at^h of th q ant ty ϕ

LEMMA 2.1 th n th s s m t ons (28) e con s d, d th $\lambda_\ell = \frac{\rho}{\rho_\ell} = \frac{\alpha_\ell}{Y_\ell}$ s mooth s o t ons of (25)–(28) s at s fy th f o o ng nt o y n q e t s

$$\partial_t \rho s_\ell + \partial_x \rho s_\ell u = -\frac{\lambda_\ell \mu_\ell}{T_\ell} (\partial_x u)^2 - \frac{\rho \epsilon}{T_\ell} \leq 0, \quad \ell = \tau, n_p. \quad (29)$$

As e con s q nc th f o o ng nt o y e anc q at ons e o t e n d

$$\frac{\beta_{n_p}}{T_{n_p}} \{ \partial_t \rho s_\ell + \partial_x \rho s_\ell u \} - \frac{\beta_\ell}{T_\ell} \{ \partial_t \rho s_{n_p} + \partial_x \rho s_{n_p} u \} = \frac{\rho \epsilon}{T_\ell T_{n_p}} (\beta_\ell - \beta_{n_p}), \quad (30)$$

fo $\tau \leq \ell \leq n_p$, τ th $\beta_\ell = \frac{\lambda_\ell \mu_\ell}{\sum_k \lambda_k \mu_k}$

f o o f th d nt ty (29) s o t e n d f o m th st on

$$\rho Y_\ell D_t e_\ell + \alpha_\ell \rho_\ell \partial_x u = \alpha_\ell \mu_\ell (\partial_x u)^2 + \rho \ell \epsilon.$$

s ng (2) and (r 5) th s st on t s s

$$-\rho Y_\ell \rho_\ell D_t v_\ell - \rho Y_\ell T_\ell D_t s_\ell + \lambda_\ell Y_\ell \rho_\ell \partial_x u = \lambda_\ell Y_\ell \mu_\ell (\partial_x u)^2 + \rho \ell \epsilon.$$

By th s s m t ons th^h $D_t v_\ell = \lambda_\ell D_t (\tau / \rho) = \frac{\lambda_\ell}{\rho} \partial_x u$ f o

$$-\rho Y_\ell T_\ell D_t s_\ell = \lambda_\ell Y_\ell \mu_\ell (\partial_x u)^2 + \rho Y_\ell \epsilon.$$

th n (29) s o^h d and (30) f o o s □

th nt o y e anc q at ons th^h st e s h d n th e o^h s t e d^h ot d to e h^h d f n f a c t e s m e s t h o d s t con c n ng th t nc 3 6 f n d, d th^h

LEMMA 2.2 th s mooth s o t ons of (25)–(28) s at s fy th f o o ng t nt n t o y st on

$$\partial_t \rho s' + \partial_x \rho s' u = \frac{\gamma' - \tau}{\rho^{\gamma' - 1}} \left(\mu' (\partial_x u)^2 - \rho \epsilon \right) \quad \text{th} \quad s' = \frac{(\gamma' - \tau) \rho k}{\rho^{\gamma'}} \quad (3r)$$

As a consequence the following equation is obtained

$$\mu' \frac{\gamma' - \tau}{\rho^{\gamma' - 1}} \{ \partial_t \rho s_{n_p} + \partial_x \rho s_{n_p} u \} - \frac{\lambda_{n_p} \mu_{n_p}}{T_{n_p}} \{ \partial_t \rho s' + \partial_x \rho s' u \} = \frac{\rho \epsilon}{T_{n_p}} \frac{\gamma' - \tau}{\rho^{\gamma' - 1}} (\mu' - \lambda_{n_p} \mu_{n_p}). \quad (32)$$

From the continuity (3^r) it follows that the volume of ρk is also

$$\frac{(\gamma' - \tau)}{\rho^{\gamma'}} \left(\partial_t (\rho k) + u \partial_x (\rho k) + \gamma' \rho k \partial_x u \right) = \frac{(\gamma' - \tau)}{\rho^{\gamma'}} \left(\mu' (\partial_x u)^2 - \rho \epsilon \right). \quad (33)$$

From the continuity hypothesis

$$(\gamma' - \tau) \rho k \left(\partial_t \frac{\tau}{\rho^{\gamma'}} + u \partial_x \frac{\tau}{\rho^{\gamma'}} - \frac{\gamma'}{\rho^{\gamma'}} \partial_x u \right) = 0. \quad (34)$$

From (33) and (34) it follows

$$\partial_t s' + u \partial_x s' = \frac{\gamma' - \tau}{\rho^{\gamma'}} \left(\mu' (\partial_x u)^2 - \rho \epsilon \right).$$

Using the relation $\rho (\partial_t s' + u \partial_x s') = \partial_t \rho s' + \partial_x \rho s' u$ the relation (3^r) is obtained. From (32) is obtained by comparison (2^o) and (3^r) \square . From the system (2^o) it is easy to deduce the following equation

$$\partial_t \frac{k^{C_1}}{\epsilon} + u \partial_x \frac{k^{C_1}}{\epsilon} = (C_2 - C_1) k^{C_1 - 1}. \quad (35)$$

In this case the variable $\frac{k^{C_1}}{\epsilon}$ is independent of $\rho \epsilon$. The system (2^o) is reduced to the system (2^o) and the continuity equation (3^r) is also added to the system (2^o) and (3^r) is added to form a non-conservative system (2^o) and the following equation is obtained

$$\begin{cases} \partial_t \rho + \partial_x \rho u = 0, \\ \partial_t \rho u + \partial_x (\rho u^2 + p + \frac{2}{3} \rho k) = \partial_x ((\mu + \mu') \partial_x u), \\ \partial_t E + \partial_x (E + p + \frac{2}{3} \rho k) u = \partial_x ((\mu + \mu') u \partial_x u), \\ \frac{\beta_{n_p}}{T_{n_p}} \{ \partial_t \rho s_\ell + \partial_x \rho s_\ell u \} - \frac{\beta_\ell}{T_\ell} \{ \partial_t \rho s_{n_p} + \partial_x \rho s_{n_p} u \} = \frac{\rho \epsilon}{T_\ell T_{n_p}} (\beta_\ell - \beta_{n_p}), \\ \frac{\lambda_{n_p} \mu_{n_p}}{T_{n_p}} \{ \partial_t \rho s' + \partial_x \rho s' u \} - \mu' \frac{\gamma' - 1}{\rho^{\gamma' - 1}} \{ \partial_t \rho s_{n_p} + \partial_x \rho s_{n_p} u \} = \frac{\rho \epsilon}{T_{n_p}} \frac{\gamma' - 1}{\rho^{\gamma' - 1}} (\lambda_{n_p} \mu_{n_p} - \mu'), \\ \partial_t \rho \frac{k^{C_1}}{\epsilon} + \partial_x \rho \frac{k^{C_1}}{\epsilon} u = (C_2 - C_1) \rho k^{C_1 - 1}, \end{cases} \quad (36)$$

Let $\tau \leq \ell \leq n_p - \tau$. According to the continuity equation the state variables s_{n_p} is not an unknown of (36) it is not to be defined on the unknowns $s_{n_p} = s_{n_p}(\rho, \rho u, E, \rho s_1, \dots, \rho s_{n_p-1}, \rho s', \rho k^{C_1} \epsilon)$

Let us assume that the viscosity functions are a product of the characteristic viscosity of the gas and a function of the state variables. Consider the following state equation

$$\lambda_{n_p} \mu_\ell = (Y_\ell T_\ell)^{m_\ell} \bar{\mu}_\ell \quad \ell \leq \ell \leq n_p,$$

where $m_\ell > 0$ are constants to be determined in the state equation and $\bar{\mu}_\ell$ is given by $(\bar{T}_\ell = Y_\ell T_\ell = \bar{p}_\ell v / (\gamma_\ell - 1))$ the values β_ℓ can be computed as follows

$$\beta_\ell = \frac{(\bar{T}_\ell)^{m_\ell} \bar{\mu}_\ell}{\sum_{1 \leq i \leq n_p} (\bar{T}_i)^{m_i} \bar{\mu}_i}. \quad (3)$$

Let β_ℓ denote the viscosity function and let us note that the constants β_ℓ are associated with $f(\mathbf{w})$ the diffusion tensor $D(\mathbf{w})$ and the source term S^C and finally

$$\mathbf{w}^C = \begin{pmatrix} \rho \\ \rho u \\ E \\ \rho Y_1 \\ \frac{\rho k^{C_1}}{\epsilon} \end{pmatrix}, \quad \mathbf{f}(\mathbf{w}) = \begin{pmatrix} \rho u \\ \rho u^2 + p + p' \\ (E + p + p')u \\ \rho Y_1 u \\ \frac{\rho k^{C_1}}{\epsilon} u \end{pmatrix},$$

$$D(\mathbf{w}) = \begin{pmatrix} 0 \\ \partial_x((\mu + \mu')\partial_x u) \\ \partial_x((\mu + \mu')u\partial_x u) \\ 0 \\ 0 \end{pmatrix}, \quad S^C(\mathbf{w}) = \begin{pmatrix} 0 \\ 0 \\ 0 \\ 0 \\ (C_2 - C_1)\rho k^{C_1-1} \end{pmatrix},$$

where $\mathbf{w} = {}^t(\mathbf{w}^C, \mathbf{w}^{NC})$ is a vector of non conserved variables \mathbf{w}^{NC} and the associated source term $S^{NC}(\mathbf{w}, \rho s_{n_p})$ and a vector $Q(\mathbf{w}, \rho s_{n_p})$ and finally

$$\mathbf{w}^{NC} = \begin{pmatrix} \rho s_1 \\ \rho s_{n_p-1} \\ \rho s' \end{pmatrix}, \quad \mathbf{g}(\mathbf{w}) = \begin{pmatrix} \rho s_1 u \\ \rho s_{n_p-1} u \\ \rho s' u \end{pmatrix},$$

$$Q(\mathbf{w}, \rho s_{n_p}) = \begin{pmatrix} \frac{\beta_1 T_{n_p}}{T_1 \beta_{n_p}} \\ \frac{\beta_{n_p-1} T_{n_p}}{T_{n_p-1} \beta_{n_p}} \\ \frac{\mu' T_{n_p} (\gamma' - 1)}{\lambda_{n_p} \mu_{n_p} \rho^{\gamma'-1}} \end{pmatrix}, \quad S^{NC}(\mathbf{w}, \rho s_{n_p}) = \begin{pmatrix} \frac{\rho \epsilon (\beta_1 - \beta_{n_p})}{T_1 \beta_{n_p}} \\ \frac{\rho \epsilon (\beta_{n_p-1} - \beta_{n_p})}{T_{n_p-1} \beta_{n_p}} \\ \frac{\rho \epsilon}{\lambda_{n_p} \mu_{n_p} (\lambda_{n_p} \mu_{n_p} - \mu')} \frac{\gamma' - 1}{\rho^{\gamma'-1}} \end{pmatrix}.$$

For the model we assume

$$\begin{cases} \partial_t \mathbf{w}^C + \partial_x \mathbf{f}(\mathbf{w}) = D(\mathbf{w}) + S^C(\mathbf{w}), \\ \partial_t \mathbf{w}^{NC} + \partial_x \mathbf{g}(\mathbf{w}) = S^{NC}(\mathbf{w}, \rho s_{n_p}) + Q(\mathbf{w}, \rho s_{n_p}) \left\{ \partial_t \rho s_{n_p} + \partial_x \rho s_{n_p} u \right\}. \end{cases} \quad (38)$$

Let us note that the steady state system given by

$$\begin{cases} \partial_t \mathbf{w}^C + \partial_x \mathbf{f}(\mathbf{w}) = 0 \\ \partial_t \mathbf{w}^{NC} + \partial_x \mathbf{g}(\mathbf{w}) = Q(\mathbf{w}, \rho s_{n_p}) \left\{ \partial_t \rho s_{n_p} + \partial_x \rho s_{n_p} u \right\}, \end{cases}$$

is hyperbolic in the given sense

$$u \pm c, \text{ where } c^2 = \sqrt{\frac{\gamma p + \gamma' p'}{\rho}}.$$

The given sense $u \pm c$ is on order of magnitude like the given $u \approx n_p + 3$ order of magnitude. According to the order 4 or 6 one can observe the structure of taking solutions. The solutions are sufficient to observe and not on of the order of solutions of the non-conservative hyperbolic system (8 or 4 or 6). The solutions are not the order of the system and focus on attention on the numerical error of the solutions.

3 Numerical approximation

This section is devoted to a nonstandard numerical method to approximate the solutions of the non-conservative system (38). The name of this method is called "non-neighborhood method" is described in [3] (see also [6]). The idea of this method is based on the section in the context of the multidimensional numerical methods as described in the following method.

Convection is defined by the system

$$\begin{cases} \partial_t \mathbf{w}^C + \partial_x \mathbf{f}(\mathbf{w}) = 0, \\ \partial_t \mathbf{w}^{NC} + \partial_x \mathbf{g}(\mathbf{w}) = Q(\mathbf{w}, \rho s_{n_p}) \left\{ \partial_t \rho s_{n_p} + \partial_x \rho s_{n_p} u \right\}, \\ \mathbf{w}(t=0, \cdot) = \mathbf{w}^n. \end{cases} \quad (39)$$

It is so-called by a non-neighborhood method. It is important to note that the non-neighborhood method can be applied to any hyperbolic system in the form (39). The name of this method is as described in the following technique.

- *Time evolution.* The given \mathbf{w}^n the following conservative system is approximated the \mathbf{w}^n as numerical data

$$\begin{cases} \partial_t \mathbf{w}^C + \partial_x \mathbf{f}(\mathbf{w}) = 0, \\ \partial_t \mathbf{w}^{NC} + \partial_x \mathbf{g}(\mathbf{w}) = 0, \\ \mathbf{w}(t=0, \cdot) = \mathbf{w}^n. \end{cases} \quad (40)$$

At the end of this section one can be deduced that $\mathbf{w}^{n+\frac{1}{3}}$

- *Nonlinear projection.* In this context the velocity is $w^{n+\frac{2}{3}}$ computed in the velocity field and the continuity equation is enforced

$$\begin{cases} \partial_t w^C = 0, \\ \partial_t w^{NC} + \partial_x g(w) = Q(w, \rho s_{n_p}) \left\{ \partial_t \rho s_{n_p} + \partial_x \rho s_{n_p} u \right\}, \\ w(t=0, \cdot) = w^{n+\frac{1}{3}}. \end{cases}$$

Let us remark that the nonlinear projection procedure enforces the consistency in the non-conservative terms and the numerical errors are of order $\mathcal{O}(\Delta t^2)$ in the case of the non-conservative odd terms since for the numerical viscosity and the discretization of the diffusion

Diffusion and source terms are taken into account by solving the system

$$\begin{cases} \partial_t w^C = D(w) + S^C(w), \\ \partial_t w^{NC} = S^{NC}(w, \rho s_{n_p}), \\ w^C(t=0, \cdot) = w^{n+\frac{2}{3}}, \end{cases} \quad (4)$$

the $w^{n+\frac{2}{3}}$ is the solution of the nonlinear problem. At the end of this step the velocity is computed w^{n+1} . In the next steps, the velocity is computed for the diffusion and source terms.

3.1 Convection step: The 1-D case

In order to solve the system (3) one can use an explicit method of order 3 or 4. In this section we consider the case of an explicit method of order 3.

considered as a set of cells I_i and time intervals $(x_{i-\frac{1}{2}}, x_{i+\frac{1}{2}})$ and the time steps t^n, t^{n+1}

$$t^n = n\Delta t \quad \text{and} \quad x_{i+\frac{1}{2}} = (i + \frac{1}{2})\Delta x,$$

the time step Δt and the cell size Δx are constant and so that the velocity w_i^n is constant in each cell I_i and not only w_i^n but also $w_h^n(x) = w_h(x, t^n)$ is the numerical solution

$$w_h^n(x) = w_i^n \quad \text{if} \quad x \in I_i.$$

and the CFL condition

$$\frac{\Delta t}{\Delta x} \max |\lambda_i(w)| \leq \frac{1}{2}, \quad (42)$$

the solution of the Cauchy problem of the system (4) is the numerical data $w_h^n(x)$ is composed by the solutions of nonlinear equations

the constant factors L and n do not depend on $w_{i+\frac{1}{2}}(\xi)$ the action of the momentary
 mass moment at $x_{i+\frac{1}{2}}$

$$w_{i+\frac{1}{2}}(\xi) = W(\xi, w_i^n, w_{i+1}^n) \quad \text{the} \quad \xi = \frac{x - x_{i+\frac{1}{2}}}{t - t^n}.$$

The Godunov method is only the action of the solution composed of
 momentary mass moments of ρ constant functions on the
 case. The scheme is a Δx Engng scheme. Let us denote the
 by

$$\phi_{i+\frac{1}{2}}^w = t \left(f(w_{i+\frac{1}{2}}(0)), g(w_{i+\frac{1}{2}}(0)) \right),$$

in the case of the conservation states

$$w_i^{n+\frac{1}{3}} = w_i^n - \frac{\Delta t}{\Delta x} \left(\phi_{i+\frac{1}{2}}^w - \phi_{i-\frac{1}{2}}^w \right). \quad (43)$$

The continuity of the system (40) $\{\rho s_2\}(w_i^{n+\frac{1}{3}})$ sets a discrete
 continuity

$$\{\rho s_2\}(w_i^{n+\frac{1}{3}}) - (\rho s_2)_i^n + \frac{\Delta t}{\Delta x} \left(\phi_{i+\frac{1}{2}}^{\rho s_2} - \phi_{i-\frac{1}{2}}^{\rho s_2} \right) \leq 0, \quad (44)$$

the

$$\phi_{i+\frac{1}{2}}^{\rho s_2} = \phi_{i+\frac{1}{2}}^\rho \tilde{s}_2(w_{i+\frac{1}{2}}(0)).$$

Moreover the positivity of $(e_1)_i^{n+\frac{1}{3}}$ and $(e_2)_i^{n+\frac{1}{3}}$ is ensured as soon as the density
 $\rho_i^{n+\frac{1}{3}}$ is positive

Therefore the set of the continuity equations associated to ρs_2 stability
 is given by the following inequality

$$\{\rho s_2\}(w_i^{n+\frac{1}{3}}) \leq \frac{\tau}{\Delta x} \int_{x_{i-1/2}}^{x_{i+1/2}} \{\rho s_2\}(w)(x, t^{n+1}) dx. \quad (45)$$

This means that the density of the continuity $\{\rho s_2\}$ stability. On
 the other hand the conservation s_1 and s' are satisfied by the Δx and
 the fluxes Δx of the case (L^2) condition. At the discrete
 the density sets the flux of the continuity equations (30) and
 (32) in the conservation states and it is not difficult to see
 the equations (30) and (32) for $(\rho s_1)_i^{n+\frac{2}{3}}$ and $(\rho s')_i^{n+\frac{2}{3}}$ are conserved

discuss the conservation of the total energy and the total mass

$$\frac{\beta_i^{n+\frac{1}{3}}}{(T_2)_i^{n+\frac{1}{3}}} \left(\{\rho s_1\}(\mathbf{w}_i^{n+\frac{2}{3}}) - (\rho s_1)_i^{n+\frac{1}{3}} \right) - \frac{\tau - \beta_i^{n+\frac{1}{3}}}{(T_1)_i^{n+\frac{1}{3}}} \left((\rho s_2)_i^{n+\frac{2}{3}} - (\rho s_2)_i^{n+\frac{1}{3}} \right) = 0, \quad (46)$$

$$\frac{(\lambda_2 \mu_2)_i^{n+\frac{1}{3}}}{(T_2)_i^{n+\frac{1}{3}}} \left(\{\rho s'\}(\mathbf{w}_i^{n+\frac{2}{3}}) - (\rho s')_i^{n+\frac{1}{3}} \right) - (\mu')_i^{n+\frac{1}{3}} \frac{\gamma' - \tau}{(\rho_i^{n+\frac{1}{3}})^{\gamma'-1}} \left((\rho s_2)_i^{n+\frac{2}{3}} - (\rho s_2)_i^{n+\frac{1}{3}} \right) = 0, \quad (47)$$

where

$$(\rho s_2)_i^{n+\frac{1}{3}} = (\rho s_2)_i^n - \frac{\Delta t}{\Delta x} \left(\phi_{i+\frac{1}{2}}^{\rho s_2} - \phi_{i-\frac{1}{2}}^{\rho s_2} \right).$$

The above non-linear problem in $(\mathbf{w}^{NC})_i^{n+\frac{2}{3}}$ can be solved to admit a unique solution as soon as the exact mass source is not defined at the discrete nodes $(\rho s_2)_i^{n+\frac{2}{3}}$ according to

$$(\rho s_2)_i^{n+\frac{2}{3}} = \{\rho s_2\}(\mathbf{w}_i^{n+\frac{2}{3}}).$$

In addition, let us consider the following

THEOREM 3.1 Let us consider the scheme (43) and the CFL condition (42) the following discrete entropy estimates

$$\begin{aligned} & \{\rho \Psi_\ell(s_\ell)\}(\mathbf{w}_i^{n+\frac{2}{3}}) - (\rho \Psi_\ell(s_\ell))_i^n \\ & + \frac{\Delta t}{\Delta x} \left\{ \{\rho \Psi_\ell(s_\ell)u\}_{i+1/2}^n - \{\rho \Psi_\ell(s_\ell)u\}_{i-1/2}^n \right\} \leq 0, \quad \ell = \tau, 2, \end{aligned}$$

for any strictly increasing functions Ψ_ℓ associated to satisfy the convexity of the mass $\mathbf{w} \rightarrow \rho \Psi_1(s_1)$ and $\mathbf{w} \rightarrow \rho \Psi_2(s_2(\mathbf{w}))$ the following mass conservation is satisfied

$$(s_\ell)_i^{n+\frac{2}{3}} \leq \text{max}((s_\ell)_{i-1}^n, (s_\ell)_i^n, (s_\ell)_{i+1}^n), \quad \ell = \tau, 2. \quad (48)$$

The above conservation laws $(e_1)_i^{n+\frac{2}{3}}$ and $(e_2)_i^{n+\frac{2}{3}}$ stay constant as soon as the density $\rho_i^{n+\frac{2}{3}}$ is constant and the mass conservation $0 \leq (Y_{1,2})_i^{n+\frac{2}{3}} \leq \tau$ is satisfied

Therefore, in the multidimensional case only the time evolution is studied from the τ case, following the numerical solution and the density at the discrete nodes

3.2 Diffusion and source terms

In this section, we do not discuss the discretization of the diffusion and source terms, and for the advection (and the reaction) terms, we use numerical methods as proposed. Concerning the source terms, we assume that the size of source terms is small compared to dynamics of the flow (given by the hydrodynamic system). For the numerical calculation, we add the following set of equations:

$$\begin{cases} \partial_t \rho = 0, & \partial_t \rho u = 0, & \partial_t \rho Y = 0, \\ \partial_t \rho \epsilon \ell = \rho \ell \epsilon, \\ \partial_t \rho k = -\rho \epsilon, \\ \partial_t \rho \epsilon = -C_2 \rho \frac{\epsilon^2}{k}. \end{cases}$$

The system is not guaranteed to be stable for $w^{n+\frac{2}{3}}$ to obtain

$$\begin{cases} \rho^{n+1} = \rho^{n+\frac{2}{3}}, & u^{n+1} = u^{n+\frac{2}{3}}, & Y^{n+1} = Y^{n+\frac{2}{3}}, \\ k^{n+1} = \left(\frac{(k^{n+\frac{2}{3}})C_2}{(C_2 - \tau)\epsilon^{n+\frac{2}{3}}\Delta t + k^{n+\frac{2}{3}}} \right)^{\frac{1}{C_2-1}}, \\ \epsilon^{n+1} = \frac{\epsilon^{n+\frac{2}{3}}k^{n+1}}{(C_2 - \tau)\epsilon^{n+\frac{2}{3}}\Delta t + k^{n+\frac{2}{3}}}, \\ e_\ell^{n+1} = e_\ell^{n+\frac{2}{3}} + (k^{n+\frac{2}{3}} - k^{n+1}), & \tau \leq \ell \leq n_p. \end{cases}$$

For the numerical stability, we consider

3.3 The 2-D extension

The main reasons that we do not solve the discrete continuity standard equations are the following: (1) -Stochastic atoms (2) system is given by

$$\begin{cases} \partial_t \mathbf{w}^C + \partial_x \mathbf{F}_1(\mathbf{w}) + \partial_y \mathbf{F}_2(\mathbf{w}) = D(\mathbf{w}) + S^C(\mathbf{w}), \\ \partial_t \mathbf{w}^{NC} + \nabla \cdot (\mathbf{G}(\mathbf{w})) = S^{NC}(\mathbf{w}, \rho s_{n_p}) + Q(\mathbf{w}, \rho s_{n_p}) \{ \partial_t \rho s_{n_p} + \nabla \cdot (\rho s_{n_p} \mathbf{u}) \}, \end{cases}$$

where

$$\mathbf{w}^C = \begin{pmatrix} \rho \\ \rho \mathbf{u} \\ E \\ \rho Y_1 \\ \frac{\rho k^{C_1}}{\epsilon} \end{pmatrix}, \quad \mathbf{F}_1(\mathbf{w}) = \begin{pmatrix} \rho u_1 \\ \rho u_1^2 + p + p' \\ \rho u_1 u_2 \\ (E + p + p')u_1 \\ \rho Y_1 u_1 \\ \frac{\rho k^{C_1}}{\epsilon} u_1 \end{pmatrix}, \quad \mathbf{F}_2(\mathbf{w}) = \begin{pmatrix} \rho u_2 \\ \rho u_1 u_2 \\ \rho u_2^2 + p + p' \\ (E + p + p')u_2 \\ \rho Y_1 u_2 \\ \frac{\rho k^{C_1}}{\epsilon} u_2 \end{pmatrix},$$

and

$$\mathbf{u} = \begin{pmatrix} u_1 \\ u_2 \end{pmatrix}, \quad \mathbf{G}(\mathbf{w}) = \begin{pmatrix} \rho s_1 \mathbf{u} \\ \rho s_{n_p-1} \mathbf{u} \\ \rho s' \mathbf{u} \end{pmatrix}.$$

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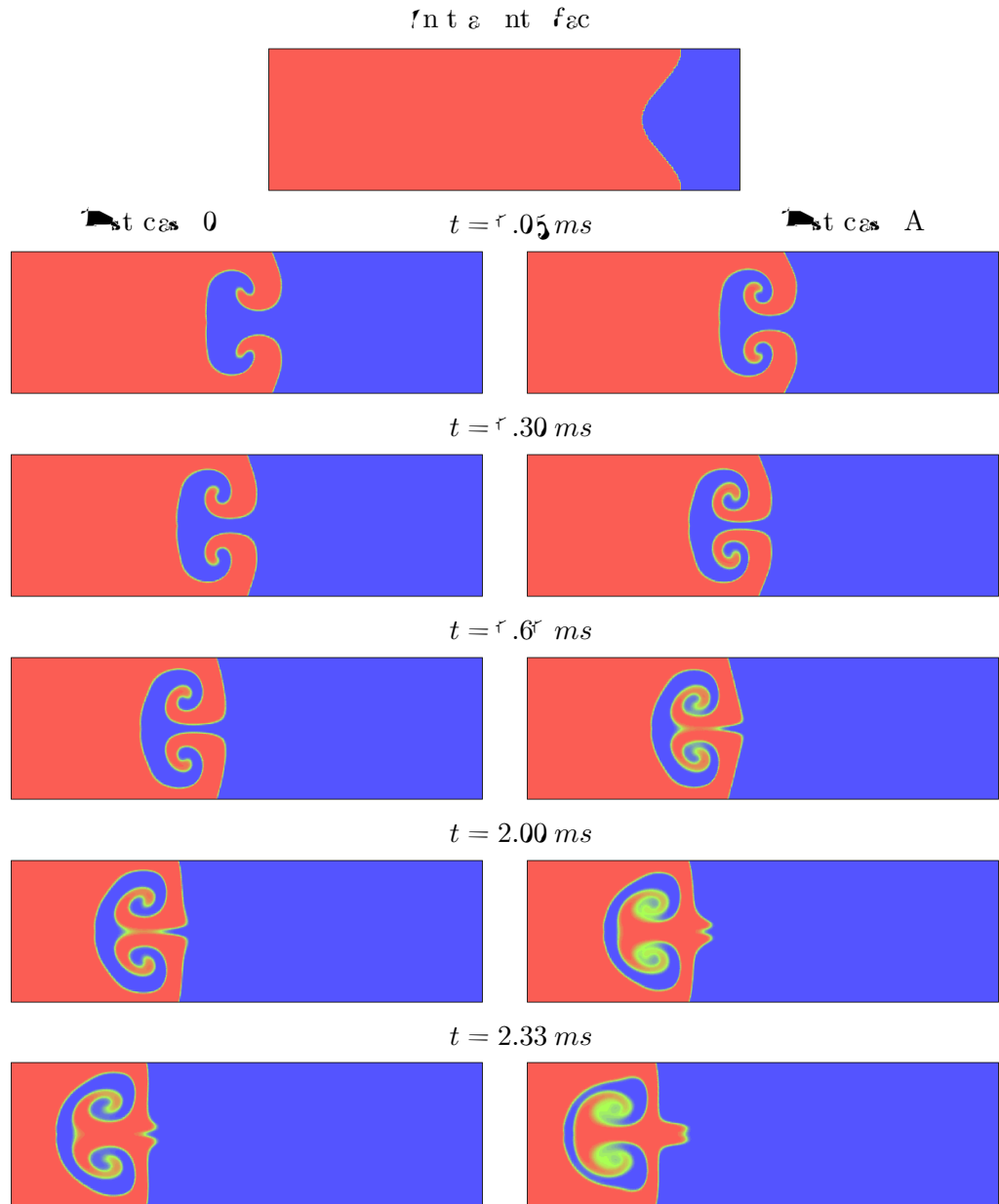


Fig. 3. Evolution of the interface between the two phases on the left of the channel -M. The initial state is shown in the top panel. The evolution of a complex front is shown in the (left) and the (right) panels at the following times: $t = 0$, $t = 0.05 \text{ ms}$, $t = 0.3 \text{ ms}$, $t = 0.6 \text{ ms}$, $t = 2.0 \text{ ms}$, $t = 2.33 \text{ ms}$.

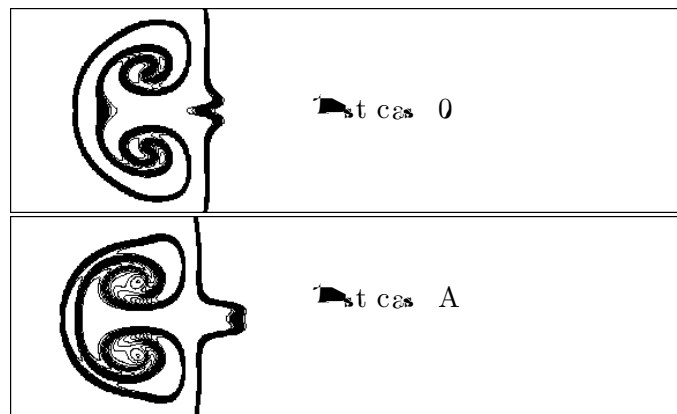


Fig. 4 Comparison of the mesh deformation of the face (defined by the same coordinate function) at the time $t = 2.33 \text{ ms}$, in two different cases: Case 0 (top) and Case A (bottom) and the resulting mesh deformation.



Fig. 5. Effects of the numerical discretization conditions on the numerical solution. The numerical solution is shown in the left panel and the corresponding contour plot is shown in the right panel. The numerical solution is shown in the left panel and the corresponding contour plot is shown in the right panel. The numerical solution is shown in the left panel and the corresponding contour plot is shown in the right panel.

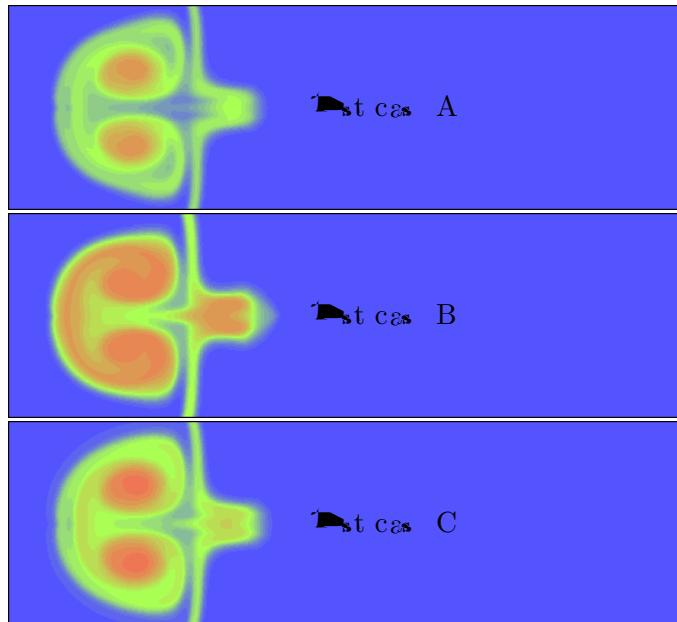


Fig. 6. Plot of density ρ_k at time $t = 2.33 \text{ ms}$ for the test cases A, B and C.